

MECHANISM OF DEGRADATION OF OLD STEEL STRUCTURE IN SUBSTATION SUBJECTED TO CORROSION AND HYDROGEN: A REVIEW

Kamal Hosen*¹, Xu Zhaodong² and Huang Xinghuai³

¹Postgraduate Student, School of Civil Engineering, Southeast University, Nanjing, China,
223217082@seu.edu.cn

²Professor, School of Civil Engineering, Southeast University, Nanjing, China,
xuzhdgyq@seu.edu.cn

³Associate Professor, School of Civil Engineering, Southeast University, Nanjing, China,
huangxh@seu.edu.cn

***Corresponding Author**

ABSTRACT

On account of cathodic protection and corrosion reactions, hydrogen can be absorbed in different amounts by steel structures during production, processing like galvanizing and pickling, and during their service life. It is widely known how hydrogen affects the tensile strength and ductility of steel parts. Although significant research has been done on the consequence effects of hydrogen on steel structures, more research is still required to examine all the pertinent factors that may affect how much hydrogen interacts with and decomposes steel. This audit examines the initial hydrogen uptake and various hazards associated with hydrogen maintained in steels. In addition, hydrogen embrittlement (HE), which occurs more frequently in steel components, is evaluated as one of the significant elements influencing the degree of hydrogen contact and debasement. Steel has changed in its mechanical characteristics as a result of extensive corrosion. Due to internal and external hydrogen, which mainly interacts with material flaws, hydrogen dissolved in metals can have an effect on their mechanical properties. Hydrogen interactions with vacancies, dislocations, grain boundaries, and other phase contacts, as well as hydrogen diffusion, dissolution, and redistribution, are some of the processes involved in this process. A typical mystery of steel structures in substations is corrosion. Through a number of methods, corrosion can cause structural failures. In severe circumstances, it may result in the complete collapse of the damaged members. It may cause steel members to lose thickness, which would reduce their structural strength. In affluent nations, the economic losses brought on by corrosion are estimated to be between three and five percent of GDP. The costs of repairing damaged equipment, materials, or buildings, backup plans, corrosion allowances, corrosion protection systems, lost productivity, environmental and health damages, etc. are all examples of corrosion losses. Products of different metallic materials are susceptible to corrosion damage, although steel constructions make up most of these products. Understanding the corrosion damage mechanism, assessing the effect on dependable services, and proposing relevant solutions are critical for preserving structures or equipment's requisite service life.

The study subjects linked to the mechanical, chemical, and physical processes involved in the mechanisms of steel structure degradation in acute environments subjected to corrosion and hydrogen are summarized in this article in the most up-to-date manner possible. This review discusses the first mechanism of corrosion degradation in various kinds of corrosion, such as uniform corrosion, pitting corrosion, and galvanized corrosion. The mechanisms of hydrogen assault, hydrogen blistering, and hydrogen embrittlement are then explored along with hydrogen uptake and changes related to absorbed hydrogen in steels.

Keywords: *Steel structure, degradation mechanism, corrosion degradation, hydrogen embrittlement, and hydrogen degradation.*

1. INTRODUCTION

There has been extensive discussion of the corrosion contrivance of high-strength steel in maritime environments (Ming Liu, 2021). According to Wang et al., consistent corrosion was the principal observation made on high-strength steel in a counterfeit coastal environment (Wang et al., 2016). The corrosion morphology was examined using an in situ 3D microscope. In their study of the corrosion compartment of high-strength withstanding steel in a pretendnaval distinctive environment, Chen found that the uniform corrosion frequency is subject to a power exponential commandment as immersion time increases and that there is an excellent correlation between the circumferential immersion corrosion test and the marine atmospheric erosion process (Wang Chen, 2016). Despite being widely recognized, iron and its alloys include a significant number of interstitial places for different hydrogen vacancies. "Dissolved hydrogen" is the name given to this hydrogen. In addition to dislocations, steels have other defects that interact with the dissolved hydrogen. Trapped hydrogen is the name given to the hydrogen found in these faults. 1864, researchers looked into the interactions between hydrogen and steel (Cailletet, 1864). Due to the far-reaching utilization of steel in mechanical implementation, the destructive impacts of hydrogen on various substances, and the predominance of hydrogen in numerous mechanical settings, these intelligent justify assist investigation (Leonard, 1993). One survey found that 25% of paraphernalia disasters in the refining industry were related to hydrogen damage in some way (P.S.A Bezerra, 1995). Different types of steel constructions can interact with hydrogen in various ways. These interactions are influenced by a number of variables, including those linked to the properties of steel or the environmental factors to which steel is subjected. When hydrogen (H) is present, a material's ability to withstand harm or bear weight suddenly disappears, a phenomenon known as hydrogen embrittlement (HE). Johnson initially recorded this occurrence in 1875 (W.H. Johnson, 1875), and it has since been noted in a variety of metallic materials, such as super alloys, Ti, Al, and iron and steel (A.J. Breen et al., 2020). Due to the ubiquity of H atoms, it is typically difficult to prevent H entry into a material, making HE a particularly dangerous embrittling phenomenon that frequently causes the catastrophic and unpredictability breakdown of large-scale engineering structures. Thus, throughout the past 100 years, the worry about HE has led to a significant number of studies (Binhan et al., 2020). A thorough examination of the various factors affecting hydrogen-related damages has not yet been undertaken. The methods of hydrogen entry into the structures of steel parts and the sources of hydrogen uptake in steel parts were discussed in this review. The degree of hydrogen interactions and damage in steels was then examined using a variety of criteria. These characteristics comprised several kinds of hydrogen-related steel defects and their most likely circumstances. Hoshihira researched the initial phase of hydrogen embrittlement and stated that when hydrogen gas is generated near a metal surface, the internal pressure increases rapidly, forming a bubble-like void beneath the metal surface that protrudes outward. (T. Hoshihira, 2009). This high pressure is influenced by the metal's ability to absorb hydrogen, the ratio of retained to dissolved hydrogen, and the temperature (Louthan, 2008). In recent years, a number of innovative methods for planning maintenance, evaluating life sequences, and designing systems of structural members have been proposed (Frangopol & Dan M., 2011) (Frangopol, 2018). These developments relate to planning, upkeep, and analyzing aging civil engineering systems. Accurately assessing the life sequence enactment of structural classifications under uncertain conditions requires a thorough understanding of the mechanisms that lead to structural degradation (Fabio & Dan M., 2018a). The effects of corrosion on steel's mechanical properties are profound. Numerous academics have conducted extensive studies on the mechanics of corrosion-damaged steel, including corrosion-damaged steel strength, corrosion-damaged steel variable modulus, corrosion-damaged steel members ductility, corrosion-damaged steel stress-strain bond (Fabio & Dan M., 2018b).

This review humorously explores steel structure degradation, featuring corrosion and hydrogen. From atmospheric and uniform corrosion to pitting, hydrogen uptake, and embrittlement, it offers a concise yet engaging overview of the challenges to structural stability.

2. DETERIORATION OF MATERIALS DUE TO CORROSION

Corrosion of steel structures is a temporal phenomenon impacted by both structural elements and environmental variables. The degree of steel corrosion is predisposed by several features, including the metal (i.e., alloy composition), the environment (temperature and relative humidity, etc.), the exposure circumstances (initial climate, housing, orientation, exposure angle, wet time, etc.), and the air pollutants, anti-icing salts, and sediments (Albrecht P. a., 1984). Corrosion has been identified as a cause of failure in studies of several bridge failures. The Point Pleasant Bridge collapsed due to non-redundant lug rails that had developed stress corrosion cracking. The hanger was knocked loose by the corrosion products in the Mianus River Bridge, which increased the load on the pins and caused fracture failure (Kulicki, 1990). The electrochemical corrosion process needs a metal, an electrolyte, and an electric current to work. To the cathode from the anode, via the electrolyte, electrons go through the base metal (in the event of a substation snow). When the positive ions produced by the anode's negative ions interact with other materials, corrosion products are created at the anode. As a result, the anode is where steel is lost. Depending on the alloying elements, different types of steel react to corrosion differently. For the necessary strength and hardness, carbon is used in mild steel, together with other alloying elements (copper, silicon, chromium, etc.). According to research (Coburn, 1968), the aforementioned environmental factors were linked to a wide range of corrosion losses in ordinary carbon steel. On each side of the plate, loss rates varied from 0.02 to 0.99 mils per year under warm temperatures and from 0.91 mils to 541 mils per year in moderate conditions. Under marine circumstances, steel materials likewise showed significant differences, with material loss ranging from 2.7 million to 28.05 million per year. Uniform corrosion, pitting, and galvanic corrosion are prevalent forms of corrosion that frequently affect steel buildings. Based on earlier studies, the mechanisms of these three types of corrosion have been explored in this section.

2.1 Characteristics and Mechanism of Atmospheric Corrosion

Numerous researchers have looked into how air pollution affects steel corrosion (D. Dasgupta, 1969). The average annual rate of steel corrosion at Derby is 6.8 mil/year, while the observed rate in Nanjing is approximately 0.2 mil/year. The central features inducing the rate of steel corrosion at Derby are high humidity and enlarged atmospheric contamination at the U.K. site. The rusting process is most likely influenced by additional elements, including temperature, precipitation, wind, radiation, surface wettability, solid particles, etc. Seasonal variations and yearly variations in the local weather conditions impact the rate of rusting in that area. Mayne discovered that when paint was applied to steel in the summer, it was more durable in terms of corrosion failure than in the winter (Mayne, 2003). When ferrous hydroxide, or $\text{Fe}(\text{OH})_2$, is exposed to oxygen throughout the rusting procedure, it quickly oxidizes to ferric hydroxide, which is more widely known as rust. Rust can be expressed mathematically as $\text{Fe}_2\text{O}_3 \cdot \text{H}_2\text{O}$ or FeOOH . Marti conducted research on the composition of air rust and discovered that it was made up of amorphous iron oxide hydrate, goethite ($\alpha\text{-FeOOH}$), magnetite (Fe_3O_4), and lepidocrocite ($\gamma\text{-FeOOH}$) (Marti B., 1963). Later, X-ray analysis of the rust that developed beneath the paint film revealed that it is primarily composed of lepidocrocite, magnetite, and haematite (Chandler and Ravee, 1966). More recently, a quantitative phase analysis discovered that, in addition to goethite, lepidocrocite, and magnetite, the rust also contains siderite, HCO_3 ions, and akaganite, Cl ions. They have some degree of protection because the oxide stage forms on the metal outward throughout the straight oxidation of iron. Iron undergoes electrochemical corrosion. However, the corrosion products often form apart from the metal and cannot inhibit the process.

2.1.1 The Notion of Crucial Humidity

The relative humidity below which corrosion stops happening is known as the critical relative humidity. In his well-known experiment, Vernon proved that iron could not corrode at 25° with a comparative humidity of fewer than 70% (W. Vernon, 1927). This might be accurate in a lab setting where no air pollutants or dust particles are present, and the original steel has not rusted. Nonetheless, research has demonstrated that if certain salts are extant on rusted steel, corrosion can happen at 40–50% comparative moisture levels. Hudson showed that there are other factors besides only having a high relative humidity that contribute to a high corrosion rate and also showed that, at relative humidities below 60%, the existence of highly hygroscopic salts in the environment can cause corrosion to begin. The duration of moisture is another determining element (W. Vernon, 1927). The amount of permitted or captivated moisture on the exposed steel surface will determine how quickly corrosion occurs, even at high relative humidity levels. Sereda invented a device to monitor the time of wetness that measured the voltage created by strictly spreading out platinum and zinc electrodes when the electrolyte was provided by surface film moisture. With this device, a relationship was formed that demonstrated how temperature and the amount of sulfur dioxide pollution in the atmosphere affected the pace at which steel corroded in the existence of oxygen and H₂O.

2.1.2 Sulphur Compounds Role in Boosting Steel Corrosion in the Atmosphere

More than six million tonnes of sulfur dioxide are thought to be released into the atmosphere each year in Britain. In the winter, gas absorption in the London area typically ranges from 0.1 to 0.2 parts per million by volume. Concentration rises significantly in a fog; in the December 2022 London smog, the absorption hit 1.4 ppm, an extremely remarkable number.

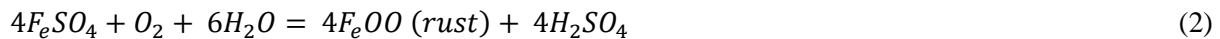
Schikorr placed forward a 3-stage progression for atmospheric steel rusting in sulphur dioxide and water (Schikorr Gerhard, 1963).

First stage: Above a specific relative humidity, rust first forms on the steel's surface. The rusty iron then absorbs SO₂ molecules, and this immersion is temperature-liberated.

In the second stage, iron and ambient Oxygen combine with the absorbed SO₂ to generate ferrous sulfate, as per the total reaction:



The third stage, known as true rusting, is caused by sulfuric acid acting as a catalyst on the ferrous sulfate created in the second stage. The general responses are as follows:



Schikorr contends that the third stage is heavily reliant on relative humidity. The response rate is relatively minimal, below about 75% relative humidity. The rate of reaction rises with temperature. When the right external factors are present, processes (2) and (3) alternate constantly and cause a significant amount of iron to corrode with minimal sulfuric acid.

2.2 Mechanism of Uniform Corrosion

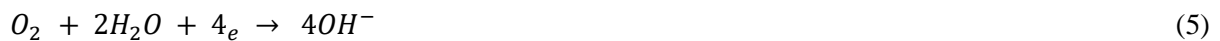
Uniform corrosion is another instance of corrosion with a very lean electrolyte layer. When only the external outward of the E690 plate is corroded, uniform corrosion slightly affects the quasi-static and low-speed effect department capability and energy captivation proficiency. However, once the inner of the plate is corroded, the powered possessions of the structure are suggestively condensed. These

findings are based on research by Ming Liu on the power-driven performance of E690 high-strength steel (Ming Liu, 2021). Even though oxygen is continuously shown within the discussion, a metal surface uncovered to the climate as it contains a restricted sum of broken down particles and water (SM, 1994). The use of corrosion inhibitors, which can act as a physical hurdle between the environment and the metal., can stop further corrosion, especially if they are insoluble like lead or copper, unlike aqueous corrosion which forms aside from the surface of metal. Ahmed authored and briefly discussed corrosion's different forms and mechanisms (Ahmad, 2006) . According to his statement, the mechanism of uniform corrosion can be expressed by the below equations:

Anodic reaction occurs at the anodic areas:



The oxygen decrease occurs in the cathodic areas:



At the anode the OH ions and Fe⁺⁺ ions combined to form:



To become Fe(OH)₃, Fe(OH)₂ oxidizes, when there is additional oxygen in the air, at which point the water is released:



Ferrous hydroxide becomes hydrated ferric oxide when exposed to oxygen, sometimes known as rust.



The following explains how water causes corrosion of steel (Figure 1).

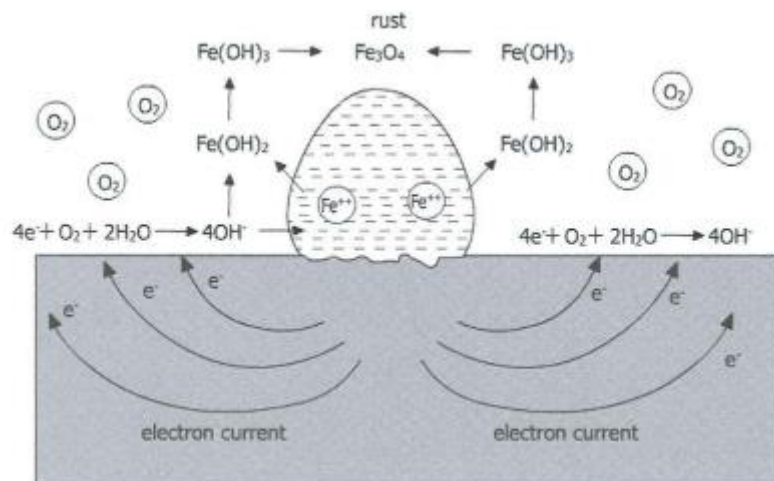


Figure 1: Iron corrodes in water (Ahmad, 2006)

In the middle of the drop zone, but not quite there, rust (Fe₂O₃·H₂O), which is alkaline, forms. In a metallic circuit, electrons move from the anode (drop center) to the cathode (periphery). The current flow is shown in Figure 1. When oxygen oxidizes ferrous ions in solution, rust comprises insoluble, hydrated ferric oxides (Ahmad, 2006).

2.3 Mechanism of Pitting Corrosion

One significant kind of localized corrosion is pitting corrosion. On a material, this kind of corrosion first appears in a comparatively limited area. Pits seem outward as the region propagates more profound and more significantly over time. Pits, also known as holes, form on the material's surface due to this kind of localized corrosion. Because less oxygen is present in an area covered in impurities or water, one functions as the anode and the other as the cathode. The metal's dissolution is thought to be caused by an electrochemical process (Hoar & Agar, 1947). Two theories are currently in widespread use: Hoar suggests the first. He connected the rise in the acidity of the solutions at the active parts to the formation and expansion of the pits (Hoar, 1949). Investigators Kabanov from Russia propose another. They connected the movement of anions away from the metal surface to the development of pits (Kabanov et al., 1947). The pitting feature is demarcated as the percentage of the inmost pit to the typical infiltration. The pitting corrosion intensity can be measured using the pitting factor. This corrosion is far more dangerous because it is tough to identify, expect, and design against. Usually, unreceptive constituents exhibit it. The corrosion is accelerated by the existence of non-uniformities. The response could go like this:

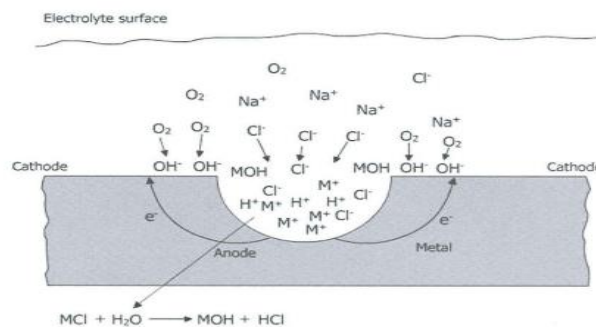


Figure 2: Diagram of metal with active corrosion pits in chloride solution (Ahmad, 2006). The oxygen reduction process begins when the entire surface comes into contact with the oxygen-containing electrolyte (Fig. 2).

3. MATERIAL DETERIORATION CAUSED BY HYDROGEN

Hydrogen can cause deterioration of steel structures through a process called hydrogen embrittlement. Hydrogen embrittlement occurs when hydrogen gas is absorbed into steel, making it brittle and prone to cracking and breaking under stress. This can occur both during the manufacturing process and during the life of the steel structure. Due to damage caused by hydrogen, pipes continuously subjected to harsh circumstances experience many failures never before seen. Different types of crack-related pipeline failures can be brought on by diffused hydrogen. Steel plates used to make pipelines are put through crucial production steps during thermo-mechanical controlled processing (TMCP) to prevent these issues (Charles, 2003).

3.1 Mechanism of Hydrogen Uptake in Steel

Zeynab conducted several kinds of research to know the system and uptake mechanism of hydrogen in steel members and stated that hydrogen can be added during the production, processing, and service life of steel (Zeynab et al., 2011). Sources of hydrogen include the interaction of steel with environmental moisture, which produces nascent hydrogen. Since all the hydrogen absorbed cannot escape into molten steel during solidification, a portion of the hydrogen atoms are deposited in voids, pores, and other interior surfaces. The steel absorbs hydrogen when exposed to hydrogen-containing acids during treatment processes like pickling (Zeynab et al., 2011). Hydrogen can also be absorbed through corrosion, cathodic protection, or the straightforward dissociation of hydrogen gas on steel surfaces while utilizing equipment containing hydrogen. Other examples of cathodic processes in alkaline solutions are water electrolysis, chlor-alkali reactions, or iron or steel hydrogen sources used as cathodes in alkaline batteries. Compared to acid solutions, alkaline solutions significantly slow down the rate at which hydrogen permeates steel. The fluctuation in the surface state and the mechanism of the hydrogen advancement reaction are responsible for this (I. Flis-Kabulska, 2007). There are now two models of hydrogen entry kinetics that are extensively used.

(a) Model for the direct hydrogen absorption process in one step. This is grounded on the notion that hydrogen comes in the metal using the same primary mechanism during discharge. This strategy might be more appropriate for metals that primarily absorb hydrogen while producing less hydrogen and acidic liquids where proton donation occurs (C. Gabrielli et al., 2006). This direct technique is effective for palladium and HY-130 steel when the hydrogen permeation current density is low (Zheng et al., 1995).

(b) Hydrogen entering the metal travels through the same metal surface adsorption states as the intermediates in the indirect penetration idea (or two-step absorption process), resulting in hydrogen evolution. Protons are allegedly reduced at the metal surface in acidic environments (Volume process).



In contrast, the H_2O dissociation in neutral or alkaline media results in the adsorbed hydrogen:



According to Heyrovsky, this adsorbed hydrogen can either undergo an electrochemical process or be converted into gaseous molecular hydrogen:



Or using a straightforward chemical recombination process (Tafel)



Where M are the adsorption sites on the metal surface, and MH_{ads} are the hydrogen adsorbed on the electrode surface.

3.2 Mechanism of Hydrogen Embrittlement

The hydrogen embrittlement theory was first proposed by Zapfe et al.. According to Zapfe's original hydrogen embrittlement theory, hydrogen atoms preferentially segregate at metal defect spots like micro gaps and inclusion sites (Zapfe et al., 1979). Hydrogen embrittlement (HE) is a well-known fact in highly strong materials. HE causes a material to fracture first, fracture further, and fail catastrophically. Thus, mechanical qualities like strength, ductility, and hardness are lost. Hydrogen

embrittlement is caused by several mechanisms, including HEDE, HELP, and AIDE. Deterioration and embrittlement are typically the result of combining these mechanisms (Sandeep and Manish, 2019). The material acquires this hydrogen through electrochemical reactions and high-pressure gaseous hydrogen environments (Vishwakarma, 2018). High-strength materials are frequently exceedingly predisposed to hydrogen embrittlement when operating in a hydrogen atmosphere. High-strength steels, high M-n steel, aluminum alloys, titanium, magnesium, and magnesium alloys are prone to HE (Liu, 2016). HE is sensitive to steels with tensile strengths more fabulous than 1000 MPa (Venezuela, 2016). The strain rate reactivity and vulnerability to delayed failure are the two fundamental characteristics of hydrogen embrittlement. Slow strain rates result in an increase in HE concentration. If we apply a higher strain rate, the material is less vulnerable to HE. Similar to this, HE components are now more prone to delayed failure. It is also commonly acknowledged that hydrogen can be moved by diffusion and dislocation in steel and alloys (Maoqiu Wang, 2007). When the connected push is lower than the abdicate quality of steel, hydrogen embrittlement, and hydrogen push splitting can lead to postponed disappointment (Zeynab et al., 2011). Steel will transfer hydrogen away from interstitial sites and towards exceptional locations when it absorbs hydrogen. Figure 3 shows the typical fastener failure by hydrogen embrittlement.



Figure 3: Typical Fastener Failure by Hydrogen Embrittlement (Ravinder & Deepak, 2014). The East Span of the Oakland Bay Bridge disastrous a test in 2013, six months before it opened. Shear bolts to the extent, experienced catastrophic disasters after just two weeks of use, which were attributed to embrittlement possibly caused by the environment (Khare et al., 2017).

3.2.1 Hydrogen-enhanced De-cohesion Mechanism and Hydrogen Enhanced Localized Plasticity.

This is the first model to explain how atomic hydrogen changes a material's characteristics. HEDE was initially described by Zaffe Sims in 1941. Increased hydrogen solubility causes hydrogen atoms to long wind quickly throughout the substantial, lowering the material's interatomic strength at the crack tip and forming cleavage-type fractures (Song J & Curtin WA, 2019; S. Ramamurthy, 2013). The most common usage of this was in 1972 when it was represented. The hydrogen atom accumulates in this close to the crack tip. Moreover, it lessens the opposition to dislodgment motion. As a result, dislocation becomes more maneuverable and functions in a metal lattice as a carrier of plastic deformation. It might be clear that it depends on the material's microstructure, stress intensity, or hydrogen clustering. A fracture graphic examination was carried out to verify the material's microstructure characteristics. HELP has a variety of structures, including HCP, BCC, and FCC types (Venezuela et al., 2018; Lynch et al., 2013).

3.2.2 Adsorption Induced Dislocation Emission and Mixed fracture

This represents the combination of HEDE and HELP. Adsorption of the solute hydrogen atoms occurs close to the fracture tip. Because of the solute hydrogen atom dislocation that forms close to the

fracture tip, hydrogen adsorption at the crack slant weakens the cohesive, strong point and interatomic bonding of materials via the HEDE process. Dislocation makes it easier for cracks to grow through the slide and for the HELP mechanism to create micro voids (Kappes et al., 2013; Nibur et al., 2016). The combined action of brittle and ductile material is known as mixed fracture. When both fracture modes interact, this kind of rupture contrivance is called an assorted rupture mechanism (Atrons et al., 2018; Depover et al., 2015).

4. CONCLUSION

Corrosion protection measures should be used for relatively lengthy service intervals to shield the structure, particularly the interior, from corrosion in a naval atmosphere. The length of corrosion significantly impacts how the E690 panel's mechanical performance changes over time. Specifically, the corrosion decreases with longer service intervals and occurs in the resulting order: external + internal > internal > external. High relative humidity, ferrous sulfate, ferrous or ferric chloride, and ammonium salts are the principal atmospheric rusting rate boosters that have been studied to date. Each of these contributes significantly to the rusting process. In an atmosphere tainted with sulfur dioxide, it makes sense for iron (II) sulfates to outweigh iron (II, III) chloride salts. The corrosion rate is most likely to be higher at industrial sites in maritime areas because a combination of ferrous and ammonium salts is projected to have a further unadorned consequence than either one alone. Vernon's crucial humidity hypothesis only holds in specific scenarios where contaminants are not present during the first phase of rusting in contaminated atmospheres. One reason for enhanced corrosion at low relative humidity could be the water-absorbing characteristics of salt-containing rusts. In terms of the actual mechanism, the electrochemical idea remains relevant. One would anticipate that the total rate of corrosion would be determined by the magnitude of a specific electrochemical reaction, either cathodic or anodic. Although the precise mode of stimulus is unclear, all the elements that cause enhanced corrosion are likely to induce either cathodic or anodic processes. Lastly, in order to develop a single theory about the mechanism, it is recommended that future research focus on ascertaining the combined impact of the contaminants on the percentage of steel corrosion. It would be beneficial to investigate the possibility of creating an inanimate or animate paint layer that can be used on rusted steel without eliminating the salt impurities. The main function of HE is to cause a material to become brittle and less ductile. The mechanical characteristics are deteriorating due to hydrogen embrittlement. Diffused hydrogen is capable of hydrogen-related disappointments, such as hydrogen embrittlement of constituents. Much obliged to progressed innovation, the consideration of HE instrument has moved from micro-scale (HEDE) to nano-scale (Offer assistance, HESIV). Deciding how plastic misshapen intuitively influences the quantitative HEDE instrument coupling between neighborhood hydrogen concentration and nuclear bond is troublesome. There is no all-inclusive component for higher instruction pertinent to all archives; instead, each existing HE instrument is, as it were, reasonable for particular materials in particular applications. However, there is no specific evidence to support these processes. Future research on hydrogen embrittlement in steel structures should concentrate on developing advanced mitigation techniques and elucidating the intricate interactions among environmental conditions, material attributes, and structural design. Priority should be given to exploring innovative materials inherently resistant to hydrogen embrittlement, advancements in early-stage detection through non-destructive testing methods, and a comprehensive approach integrating experimental investigations, computational modeling, and practical application trials. This focused strategy will contribute substantively to refining durable steel structures in hydrogen-rich environments.

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